Wave-Structure interaction in shallow water

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HYWEC 2, Bordeaux, 2019

Outline

• General approach

General approach



Floating device: ship or wave energy convertor

General approach



Floating device: ship or wave energy convertor

Notation

If f is defined on \mathbb{R}^d , we write

$$f_{i} = f_{\mid_{\mathcal{I}}}$$

In the fluid domain
$$\Omega_t$$

 $\partial_t \mathbf{U} + \mathbf{U} \cdot \nabla_{X,z} \mathbf{U} = -\frac{1}{\rho} \nabla_{X,z} P - g \mathbf{e}_z$
div $\mathbf{U} = 0$,
curl $\mathbf{U} = 0$

In the fluid domain
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curl $\mathbf{U} = 0$
At the surface

$$\forall X \in \mathcal{E}(t), \qquad \underline{P}(t, X) = P_{\mathrm{atm}},$$

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At the surface

$$\begin{array}{l} \forall X \in \mathcal{E}(t), \\ \forall X \in \mathbb{R}^{d}, \end{array} \qquad \underline{P}(t, X) = P_{\mathrm{atm}}, \\ \partial_{t} \zeta - \underline{U} \cdot N = 0 \end{array}$$

At the bottom

$$U_b\cdot N_b=0.$$

,

In the fluid domain
$$\Omega_t$$

 $\partial_t \mathbf{U} + \mathbf{U} \cdot \nabla_{X,z} \mathbf{U} = -\frac{1}{\rho} \nabla_{X,z} P - g \mathbf{e}_z$
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At the bottom

$$U_b \cdot N_b = 0.$$

Constraint in the interior domain

The surface of the fluid coincides with the wetted portion of the body

$$\zeta_{\rm i} = \zeta_{\rm w}$$

,

Coupling(s)

Interior/Exterior coupling on $\Gamma(t) := \partial \mathcal{I}(t) = \partial \mathcal{E}(t)$ Continuity of the surface elevation and of the surface pressure

 $\zeta(t,\cdot) = \zeta_{i}(t,\cdot)$ and $\underline{P}(t,\cdot) = \underline{P}_{i}(t,\cdot)$ on $\Gamma(t)$

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Fluid/Solid coupling

Newton's equations:

$$\begin{cases} m\dot{U}_{G} = -mg\mathbf{e}z + \int_{I(t)}(P_{i} - P_{atm})N_{w}, \\ \frac{d}{dt}(\mathcal{I}\omega) = \int_{I(t)}(P_{i} - P_{atm})\mathbf{r}_{G} \times N_{w}. \end{cases}$$

Summary of the general approach

- Euler equations with
 - Free surface, constrained pressure in the exterior domain
 - Constrained surface, free pressure in the interior domain
- Oupling conditions at the contact line
- Sluid/solid coupling via Newton's equations

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Remark

The same approach can be used with (simpler) asymptotic models:

1*D* shallow water models

→ Free boundary problem for the contact line

- ID shallow water models and vertical walls → Coupling conditions at the contact line
- ID Boussinesq models
 - → Dispersive boundary layer

In the exterior domain

$$\begin{cases} \partial_t H + \partial_x Q = 0, \\ \partial_t Q + \partial_x (\frac{1}{H}Q^2 + \frac{1}{2}gH^2) = \frac{1}{\rho}H\partial_x\underline{P}_{atm} = 0 \end{cases}$$

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In the interior domain $\mathcal{I} = (x_{-}(t), x_{+}(t))$

$$\begin{cases} \partial_x Q_i = -\partial_t H_i, \\ \partial_t Q_i + \partial_x (\frac{1}{H_i} Q_i^2 + \frac{1}{2} g H_i^2) = -\frac{1}{\rho} H_i \partial_x \underline{P}_i. \end{cases}$$

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Coupling conditions at $x = x_{\pm}(t)$

 $H(t,\cdot) = H_{i}(t,\cdot), \qquad Q(t,\cdot) = Q_{i}(t,\cdot), \quad \text{ and } \quad \underline{P}_{\mathrm{atm}}(t,\cdot) = \underline{P}_{i}(t,\cdot).$

In the exterior domain

$$\begin{cases} \partial_t H + \partial_x Q = 0, \\ \partial_t Q + \partial_x (\frac{1}{H}Q^2 + \frac{1}{2}gH^2) = \frac{1}{\rho}H\partial_x \underline{P}_{atm} = 0 \end{cases}$$

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Coupling conditions at $x = x_{\pm}(t)$

$$H(t,\cdot)=H_{\mathrm{i}}(t,\cdot),\qquad Q(t,\cdot)=Q_{\mathrm{i}}(t,\cdot),\quad \text{ and }\quad \underline{P}_{\mathrm{atm}}(t,\cdot)=\underline{P}_{\mathrm{i}}(t,\cdot).$$

Coupling with the solid equations: the case of a fixed solid

$$\partial_t H_{i} = 0 \quad \rightsquigarrow \quad Q_{i}(t, x) = q_{i}(t)$$

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• Interior equations

$$\begin{cases} Q(t,x) = q_{i}, \\ \partial_{t}Q + \partial_{x}(\frac{1}{H}Q^{2} + \frac{1}{2}gH^{2}) = -\frac{1}{\rho}H\partial_{x}\underline{P}_{i} \end{cases}$$

with $\underline{P}_{i}(t, x_{\pm}(t)) = P_{\text{atm}}$

 \leadsto Solvability condition for $\underline{P}_i~(\int_{x_-}^{x_+}\partial_x\underline{P}_i=0~)$

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 \leadsto Solvability condition for \underline{P}_i ($\int_{x_-}^{x_+} \partial_x \underline{P}_i = 0$)

$$\partial_t q_{\mathbf{i}} = F(q_{\mathbf{i}}, x_+(t), x_-(t))$$

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$$\partial_t q_i = F(q_i, x_+(t), x_-(t))$$

• The problem is reduced to

$$\begin{cases} \partial_t H + \partial_x Q = 0, \\ \partial_t Q + \partial_x (\frac{1}{H}Q^2 + \frac{1}{2}gH^2) = 0 \end{cases} \quad \text{in} \quad E(t) \end{cases}$$

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with $\underline{P}_{i}(t, x_{\pm}(t)) = P_{\text{atm}}$ \rightsquigarrow Solvability condition for $\underline{P}_{i} \left(\int_{x}^{x_{\pm}} \partial_{x} \underline{P}_{i} = 0 \right)$

$$\partial_t q_i = F(q_i, x_+(t), x_-(t))$$

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 $H(t, x_{\pm}(t)) = H_{i}(t, x_{\pm}(t))$ (free boundary equation)

1D shallow water equations and vertical walls



Fixed object with vertical sidewalls at $x_{\pm} = \pm R$

Equations in the exterior and interior domains Unchanged: standard NSW equations (with pressure source term in \mathcal{I})

1D shallow water equations and vertical walls



Fixed object with vertical sidewalls at $x_{\pm} = \pm R$

Equations in the exterior and interior domains

Unchanged: standard NSW equations (with pressure source term in \mathcal{I})

Coupling conditions at $\mathbf{x} = \pm R$ $H/(t/)/H/H/(t/), \qquad Q(t, \cdot) = Q_i(t, \cdot), \quad \text{and} \quad P/(t/t/)/H/P/(t/t/).$

1D shallow water equations and vertical walls



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Equations in the exterior and interior domains

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Coupling with the solid equations: the case of a fixed solid Unchanged

Non Vertical vs Vertical wals

Non vertical walls

- Continuity of $Q \rightsquigarrow$ Boundary condition for the exterior equations
- Continuity of $H \rightsquigarrow$ Evolution equation for x_{\pm}
- Continuity of $P \rightsquigarrow$ Evolution equation for q_i

Vertical walls

- Continuity of Q → Boundary condition for the exterior equations
- Continuity/ $\phi f/H \rightsquigarrow x_{\pm} = \pm R$ are fixed!
- Continuity/ $\phi f/P \rightarrow$ Evolution equation for q_i ????

$$\begin{cases} \partial_t \zeta + \partial_x Q = 0, \\ \partial_t Q + \partial_x (\frac{1}{H}Q^2 + \frac{1}{2}gH^2) = -\frac{1}{\rho}H\partial_x \underline{P} \end{cases}$$

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• Local conservation of energy

with

$$\partial_t \mathfrak{e} + \partial_x \mathfrak{F} = 0$$

 $\mathfrak{e} = \frac{1}{2} (g\zeta^2 + \frac{1}{H}Q^2) \quad \text{and} \quad \mathfrak{F} = Q (\zeta + \frac{1}{2}\frac{Q^2}{h^2})$

$$\begin{cases} \partial_t \zeta + \partial_x Q = 0, \\ \partial_t Q + \partial_x (\frac{1}{H}Q^2 + \frac{1}{2}gH^2) = -\frac{1}{\rho}H\partial_x \underline{P} \end{cases}$$

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$$\mathfrak{e} = rac{1}{2} \left(g \zeta^2 + rac{1}{H} Q^2
ight)$$
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• Total Energy

w

$$E_{\rm tot} = \int_{\mathcal{E}} \mathfrak{e} + \frac{1}{2} \int_{\mathcal{I}} \left(g \zeta_{\rm w}^2 + \frac{q_{\rm i}^2}{h_{\rm w}} \right)$$

$$\begin{cases} \partial_t \zeta + \partial_x Q = 0, \\ \partial_t Q + \partial_x (\frac{1}{H}Q^2 + \frac{1}{2}gH^2) = -\frac{1}{\rho}H\partial_x \underline{P} \end{cases}$$

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$$E_{\mathrm{tot}} = \int_{\mathcal{E}} \mathfrak{e} + rac{1}{2} \int_{\mathcal{I}} \left(g \zeta_{\mathrm{w}}^2 + rac{q_{\mathrm{i}}^2}{h_{\mathrm{w}}}
ight)$$

Conservation of total energy

$$\mathbf{0} = \llbracket \mathfrak{F} \rrbracket + \alpha \boldsymbol{q}_{\mathrm{i}} \dot{\boldsymbol{q}}_{\mathrm{i}}$$

• Evolution equation for q_i

$$lpha \dot{q}_{\mathrm{i}} = - \llbracket \zeta + rac{1}{2} rac{q_{\mathrm{i}}^2}{h_{\mathrm{w}}^2}
rbracket.$$



Fixed object with vertical sidewalls at $x_{\pm} = \pm R$



Fixed object with vertical sidewalls at $x_{\pm} = \pm R$

$$\begin{cases} \partial_t \zeta + \partial_x q = 0, \\ (1 - \delta^2 \partial_x^2) \partial_t q + \varepsilon \partial_x (\frac{1}{h_0} q^2) + h \partial_x \zeta = -h \partial_x \underline{P} \end{cases}$$

with

$$\begin{cases} \underline{P} = P_{\mathrm{atm}} & \text{ on } \mathcal{E} = (-\infty, -R) \cup (R, \infty) \\ \zeta = \zeta_{\mathrm{w}}(x) & \text{ on } \mathcal{I} = (-R, R), \end{cases}$$



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and one coupling condition

<

$$q(t,\pm R)=q_{\rm i}(t).$$



Fixed object with vertical sidewalls at $x_{\pm} = \pm R$

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and one coupling condition

$$q(t,\pm R)=q_{\rm i}(t).$$

and, with an energy conservation argument,

$$-\alpha \dot{\boldsymbol{q}}_{\mathrm{i}} = \left[\!\left[\zeta + \varepsilon \frac{1}{2} \zeta^2 - \delta^2 \partial_x \partial_t \boldsymbol{q}\right]\!\right]$$

$$\begin{cases} \partial_t \zeta + \partial_x q = 0, \\ (1 - \delta^2 \partial_x^2) \partial_t q + \underbrace{\varepsilon \partial_x (\frac{1}{h_0} q^2) + h \partial_x \zeta}_{:=\Gamma} = 0 \quad \text{if } |x| > R \end{cases}$$

with transmission conditions

$$\begin{cases} \partial_t \zeta + \partial_x q = 0, \\ (1 - \delta^2 \partial_x^2) \partial_t q + \underbrace{\varepsilon \partial_x (\frac{1}{h_0} q^2) + h \partial_x \zeta}_{:=\Gamma} = 0 \quad \text{if } |x| > R \end{cases}$$

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• Denote R_0 the inverse of $(1 - \delta^2 \partial_x^2)$ with Dirichlet BC at $x = \pm R$,

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• $\partial_t \partial_x q(\pm R) = -\partial_x R_0 \Gamma \mp \frac{1}{\delta} \dot{q}^i$

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• $\partial_t \partial_x q(\pm R) = -\partial_x R_0 \Gamma \mp \frac{1}{\delta} \dot{q}^i$ • $\partial_t [\![\partial_x q]\!] = -[\![\partial_x R_0 \Gamma]\!] - \frac{2}{\delta} \dot{q}^i$

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with transmission conditions

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• Denote R_0 the inverse of $(1 - \delta^2 \partial_x^2)$ with Dirichlet BC at $x = \pm R$,

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•
$$\partial_t \partial_x q(\pm R) = -\partial_x R_0 \Gamma \mp \frac{1}{\delta} \dot{q}^i$$

• $\partial_t [\![\partial_x q]\!] = -[\![\partial_x R_0 \Gamma]\!] - \frac{2}{\delta} \dot{q}^i$

• Use second transmission condition

$$\dot{q}_{\mathrm{i}} = \frac{1}{\alpha + 2\delta} \left(\delta^{2} \llbracket -\partial_{x} R_{0} \Gamma \rrbracket - \llbracket \zeta + \varepsilon \frac{1}{2} \zeta^{2} \rrbracket \right)$$

An ODE!

with

$$\begin{cases} \partial_t \zeta + \partial_x q = 0, \\ \partial_t q + R_0 \partial_x \left(\varepsilon \frac{q^2}{h} + \frac{1}{2\varepsilon} (h^2 - 1) \right) = \dot{q}_i \exp(-\frac{|x|_R}{\delta}) \\ \dot{q}_i = \frac{1}{\alpha + 2\delta} \left(\delta^2 \llbracket - \partial_x R_0 \Gamma \rrbracket - \llbracket \zeta + \varepsilon \frac{1}{2} \zeta^2 \rrbracket \right) \end{cases}$$

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Remark

with

Can be put in conservative form

$$R_0\partial_x=\partial_xR_1$$

where R_1 is the inverse of $(1 - \delta^2 \partial_x^2)$ with Neumann BC.

An ODE!

$$\begin{cases} \partial_t \zeta + \partial_x q = 0, \\ \partial_t q + R_0 \partial_x \left(\varepsilon \frac{q^2}{h} + \frac{1}{2\varepsilon} (h^2 - 1) \right) = \dot{q}_i \exp(-\frac{|x|_R}{\delta}) \\ \dot{q}_i = \frac{1}{\alpha + 2\delta} \left(\delta^2 \llbracket - \partial_x R_0 \Gamma \rrbracket - \llbracket \zeta + \varepsilon \frac{1}{2} \zeta^2 \rrbracket \right) \end{cases}$$

Remark

with

Can be put in conservative form

$$R_0\partial_x = \partial_x R_1$$

where R_1 is the inverse of $(1 - \delta^2 \partial_x^2)$ with Neumann BC.

Remark

Same approach works for generating boundary conditions: solve the Boussinesq equations on $(0, \infty)$ given an initial data and $\zeta(t, x = 0)$.

References:

General approach:

- D. L. On the dynamics of floating structures, 2017

Shallow water:

- 1D, non vertical walls: T. IGUCHI, D. L., Hyperbolic free-boundary problems and applications, 2018

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- 1D, relaxation approximation, E. GODLEWSKI, M. PARISOT, J. SAINTE-MARIE, F. WAHL, Congested shallow water model: roof modelling in free surface flow, 2018.

- 2D radial, vertical walls: E. BOCCHI, Floating objects in shallow water with a radial symmetry, 2018

Boussinesq:

- Direct numerical coupling, JIANG, Ships waves in shallow water, 2001

- Direct numerical coupling, U. BOSI, A.P. ENGSIG-KARUP, C. ESKILSSON, M. RICCHIUTO, An efficient unified spectral element Boussinesq model for a point absorber, 2018

- Dispersive boundary layer approach, D. BRESCH, D. L., G. MÉTIVIER, Waves interacting with a partially immersed obstacle in the Boussinesq regime, 2018

- Application to generating BC: D. L., L. WEYNANS, Generating boundary conditions for a Boussinesq system, 2018.

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Thanks for your attention